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(54) **DATA DRIVER, ORGANIC LIGHT EMITTING DISPLAY DEVICE USING THE SAME, AND METHOD OF DRIVING THE ORGANIC LIGHT EMITTING DISPLAY DEVICE**

(75) Inventors: **Do Hyung Ryu**, Suwon (KR); **Bo Yong Chung**, Seoul (KR); **Hong Kwon Kim**, Euiwang (KR); **Oh Kyong Kwon**, Seoul (KR)

(73) Assignees: **Samsung Display Co., Ltd.**, Yongin-si (KR); **IUCF-HYU (Industry-University Cooperation Foundation Hanyang University)**, Seongong-gu (KR)

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345/80; 345/81; 345/82; 345/83

(58) **Field of Classification Search**
USPC **345/76-83**
See application file for complete search history.

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Primary Examiner — Sumati Lefkowitz

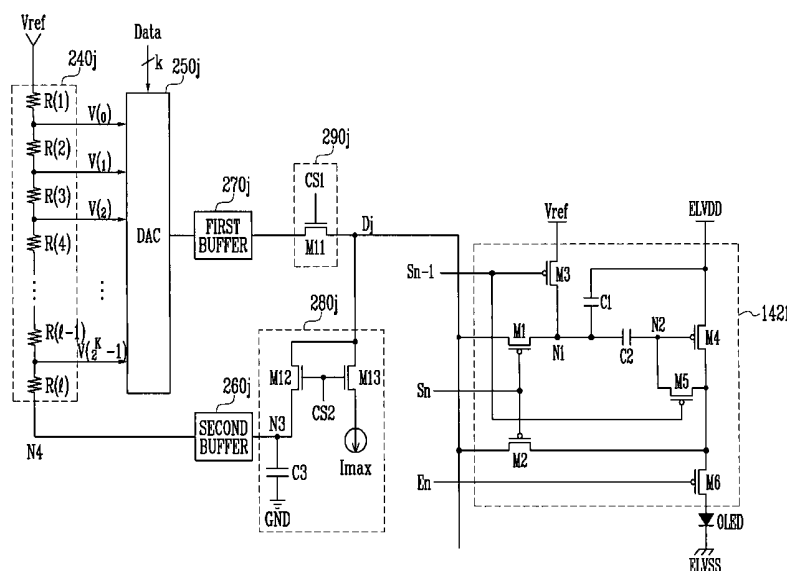
Assistant Examiner — Andrew Yeretsky

(74) *Attorney, Agent, or Firm* — Christie, Parker & Hale, LLP

(57) **ABSTRACT**

A data driver capable of displaying images with a substantially uniform brightness, an organic light emitting display device using the same, and a method of driving the organic light emitting display device. The data driver includes a plurality of current sink units for controlling predetermined currents to flow through data lines, a plurality of voltage generators for resetting values of gray scale voltages using compensation voltages generated when the predetermined currents flow, a plurality of digital-to-analog converters for selecting one gray scale voltage among the gray scale voltages as a data signal in response to bit values of the data supplied from the outside, and a plurality of switching units for supplying the data signal to the data lines. The predetermined currents may be set equal to pixel currents that correspond to a maximum brightness.

16 Claims, 13 Drawing Sheets



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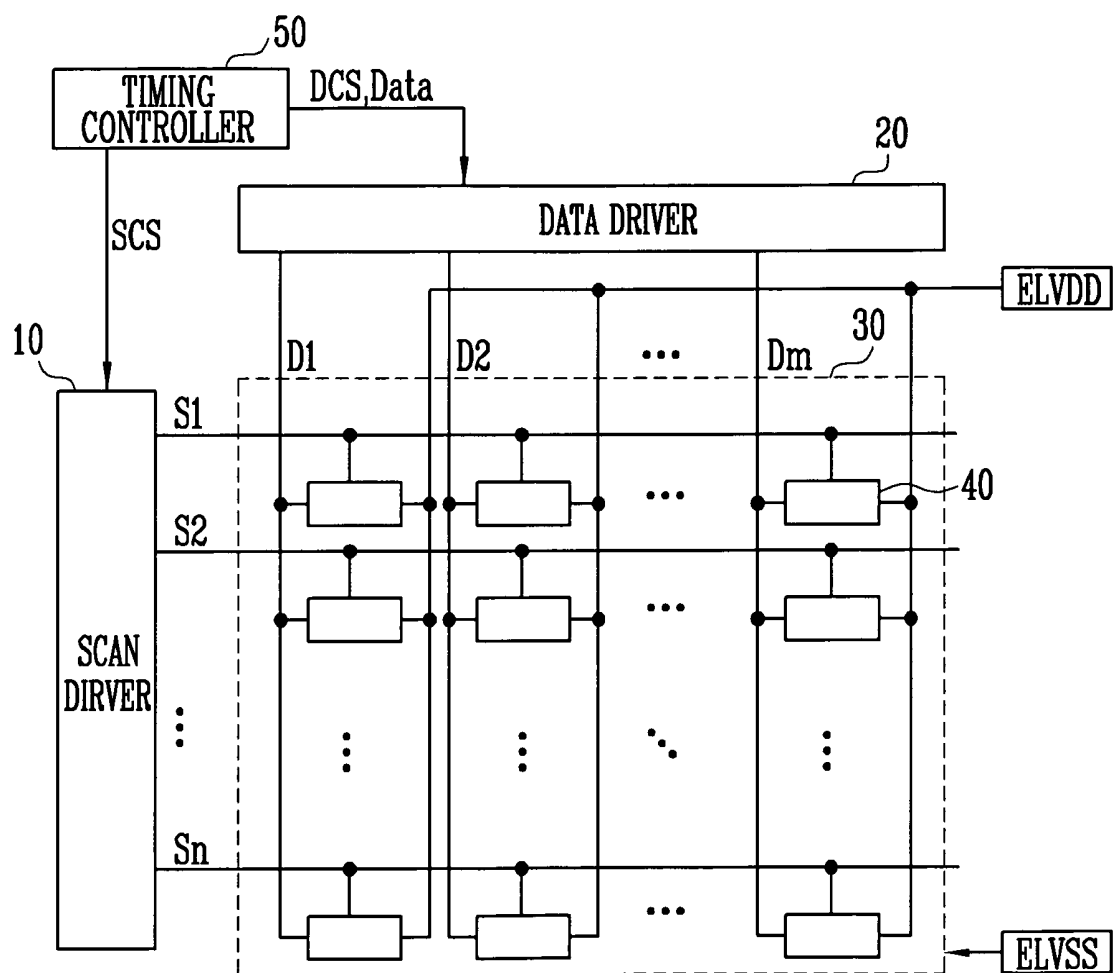
FIG. 1
(PRIOR ART)

FIG. 2

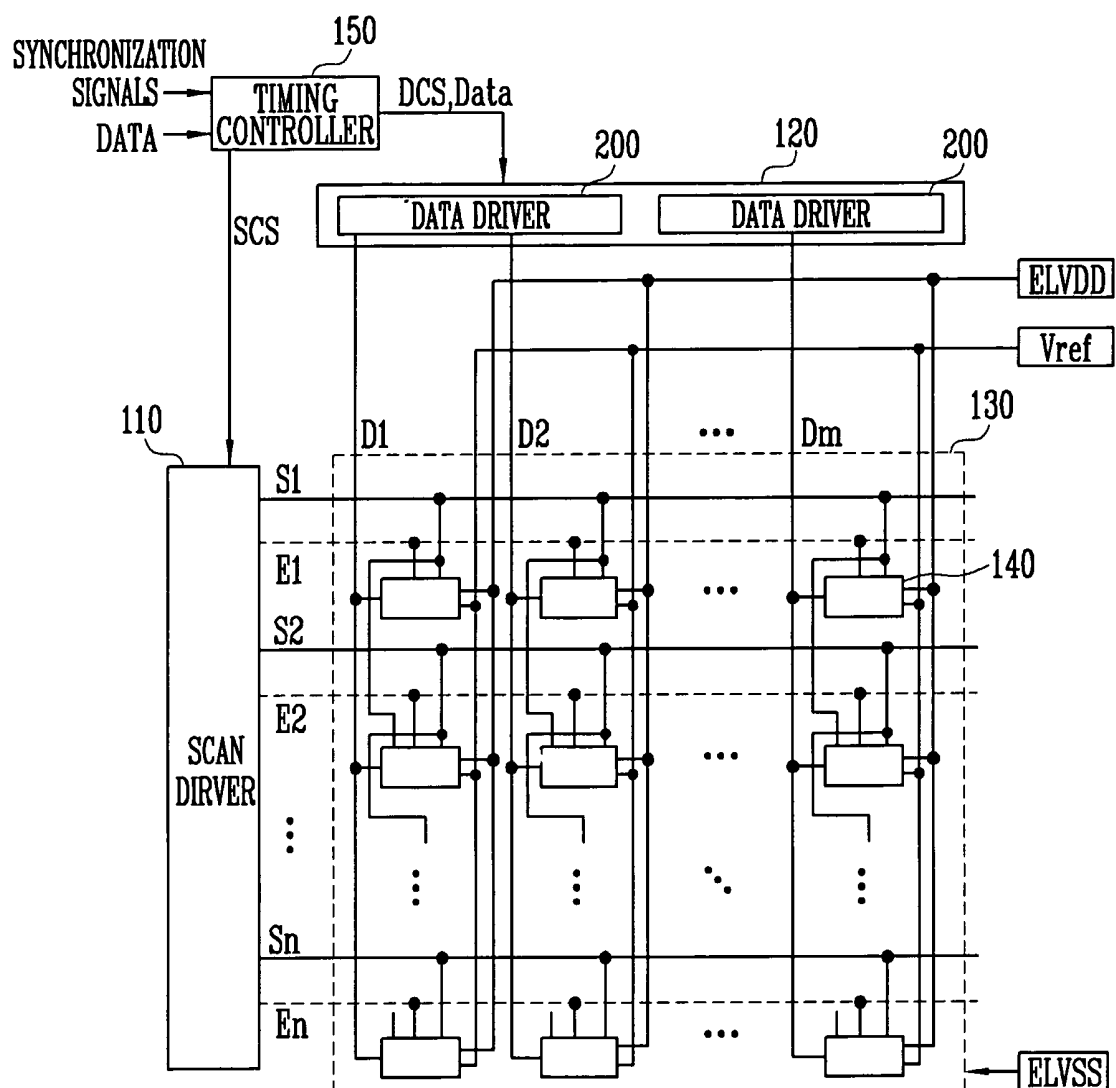


FIG. 3

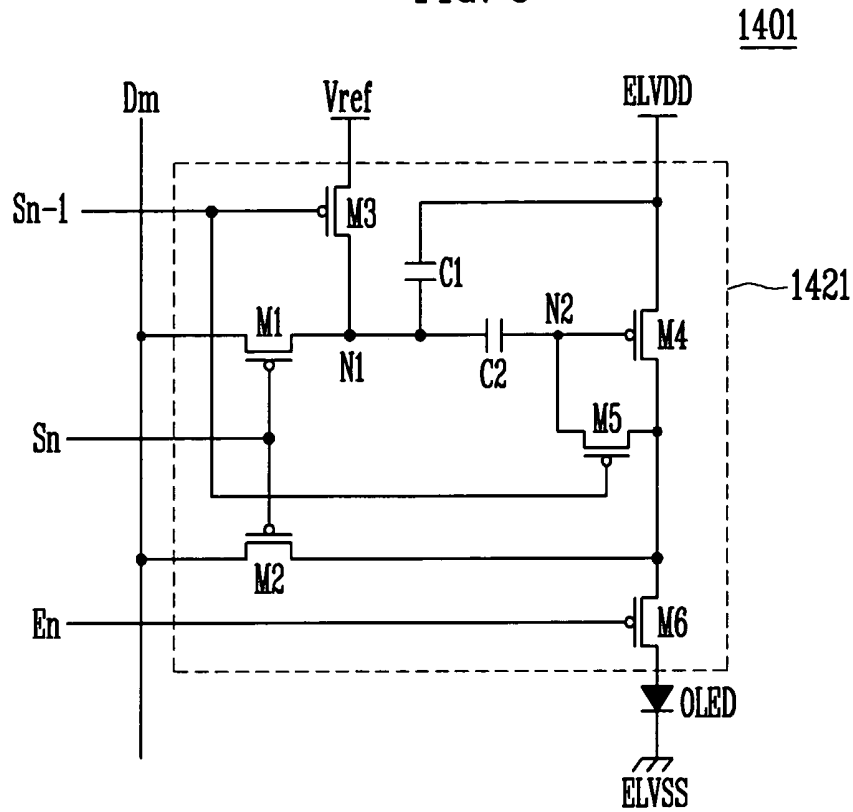


FIG. 4

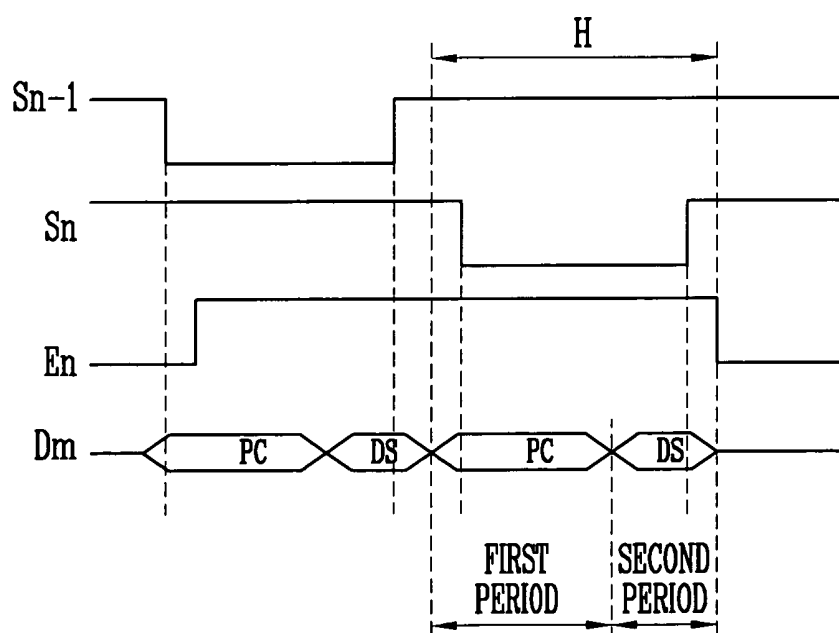


FIG. 5

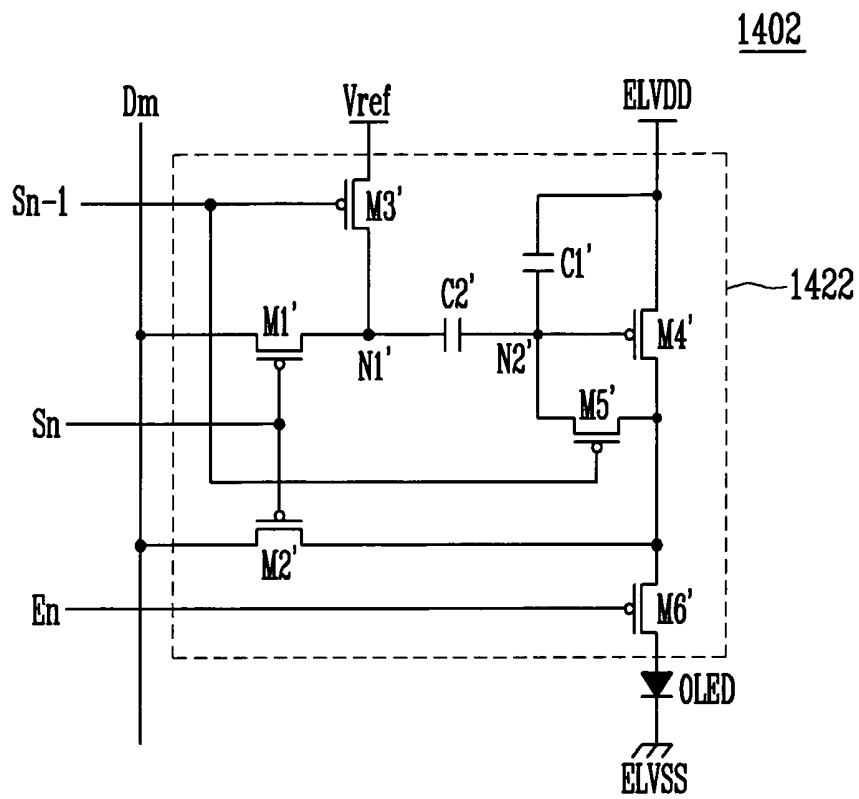


FIG. 6

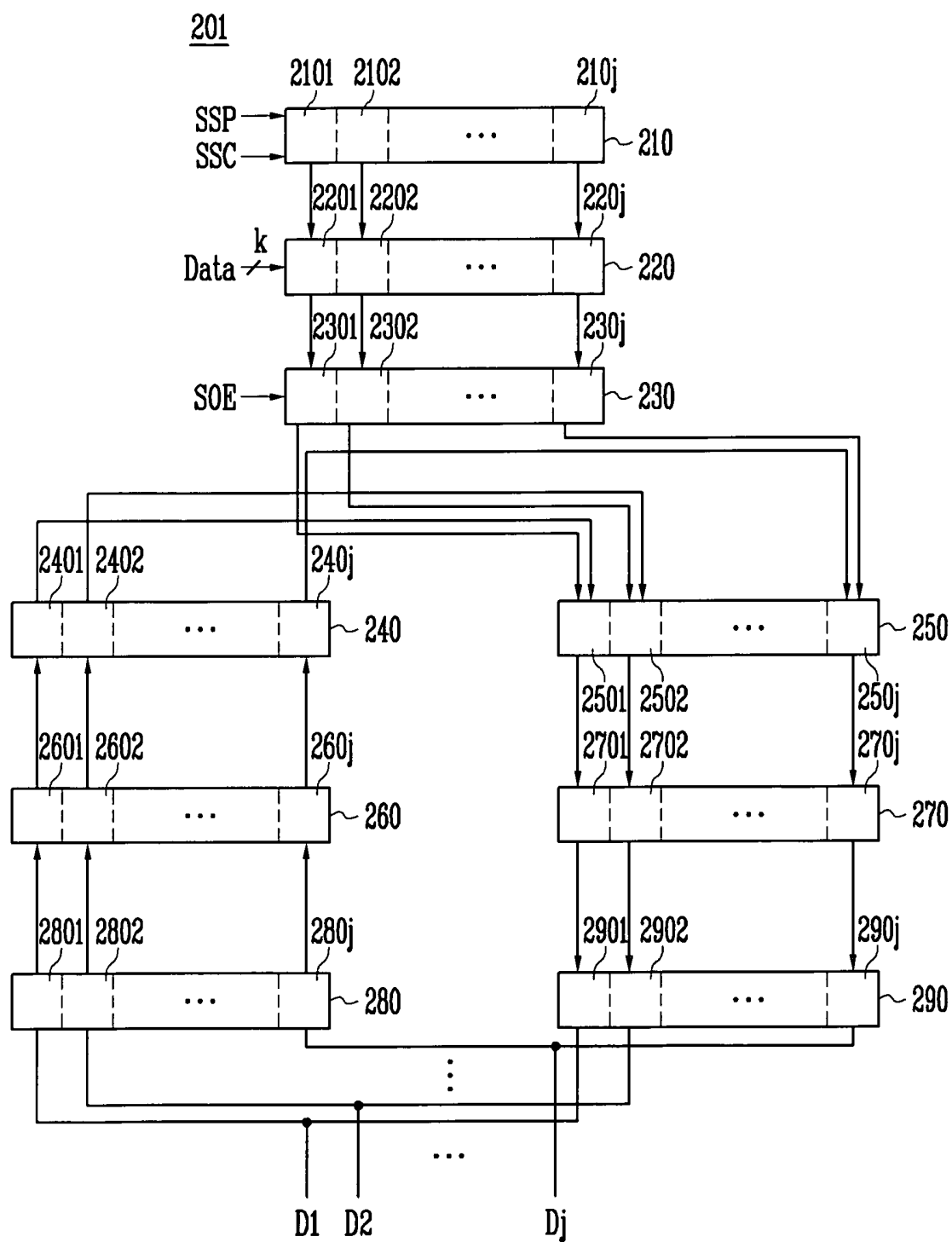


FIG. 7

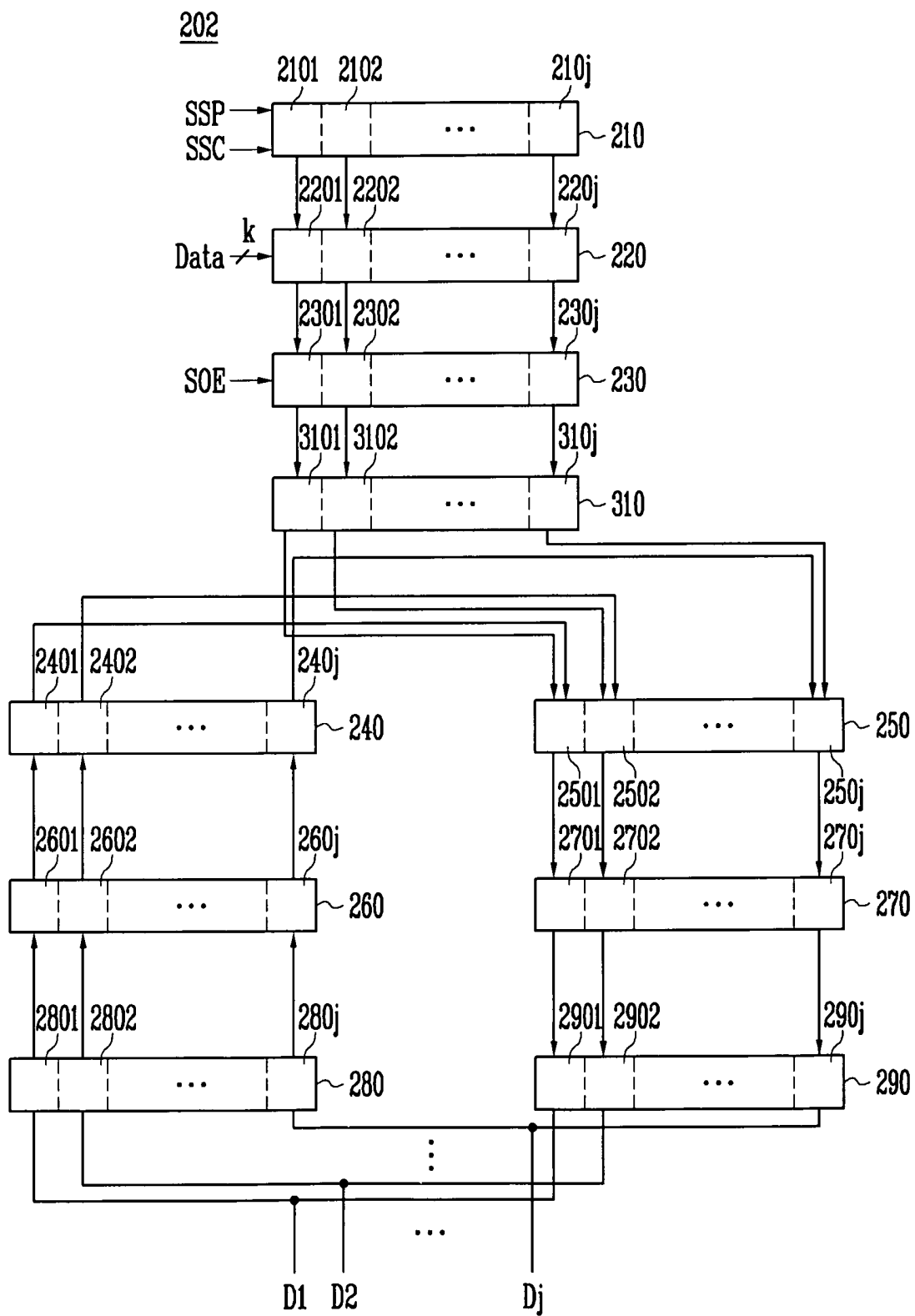


FIG. 8

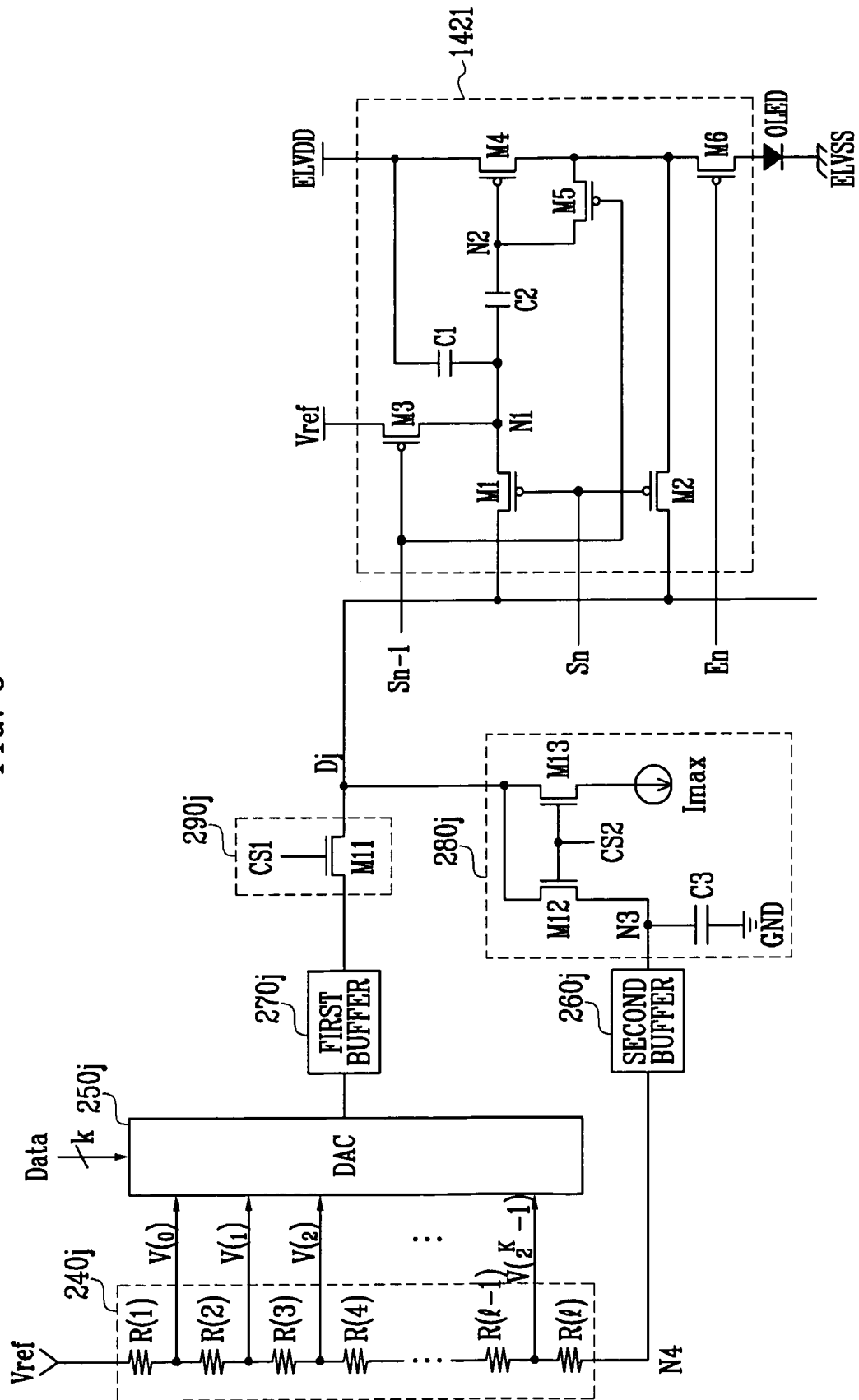


FIG. 9

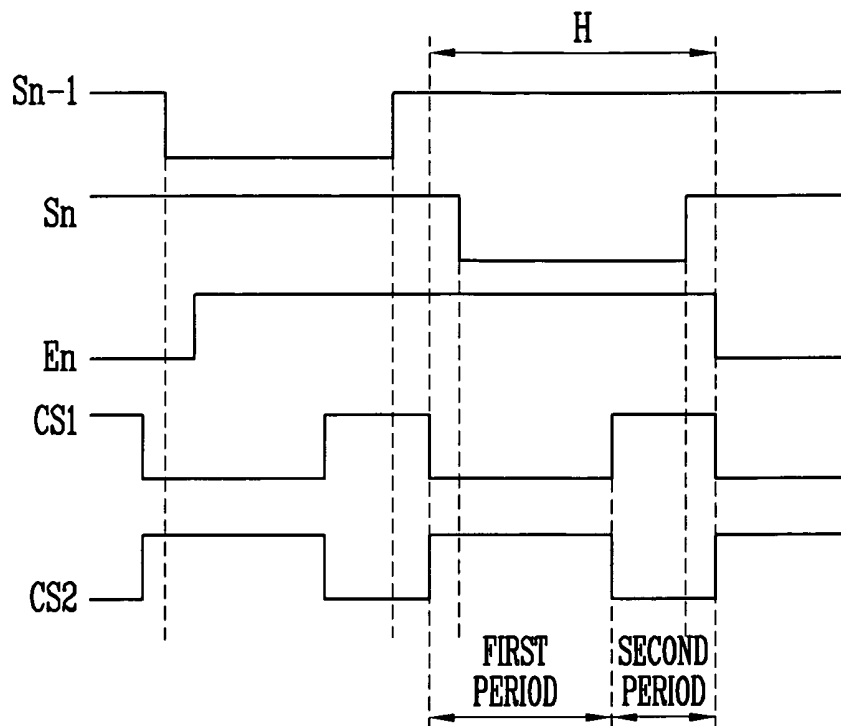


FIG. 12

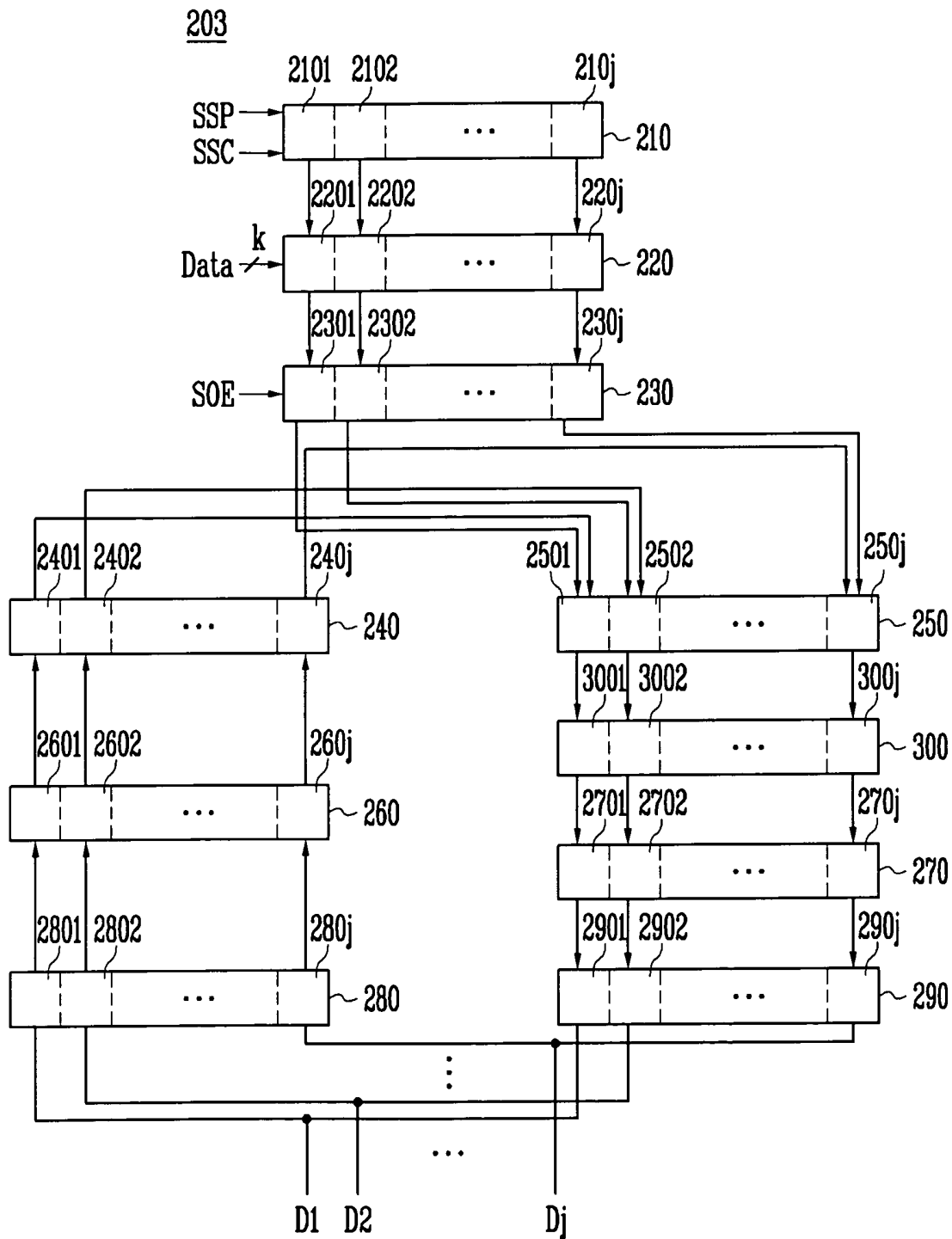


FIG. 13

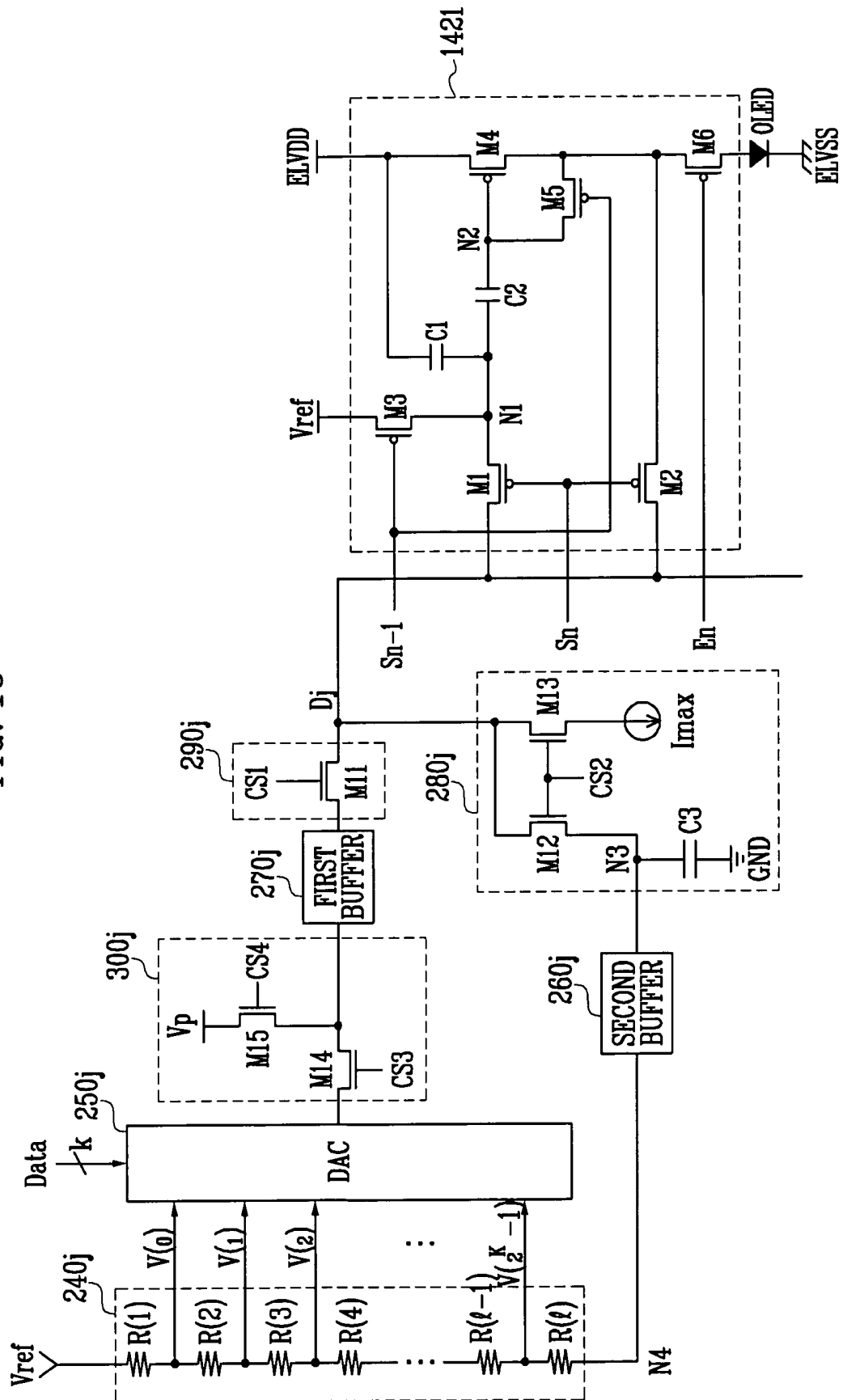
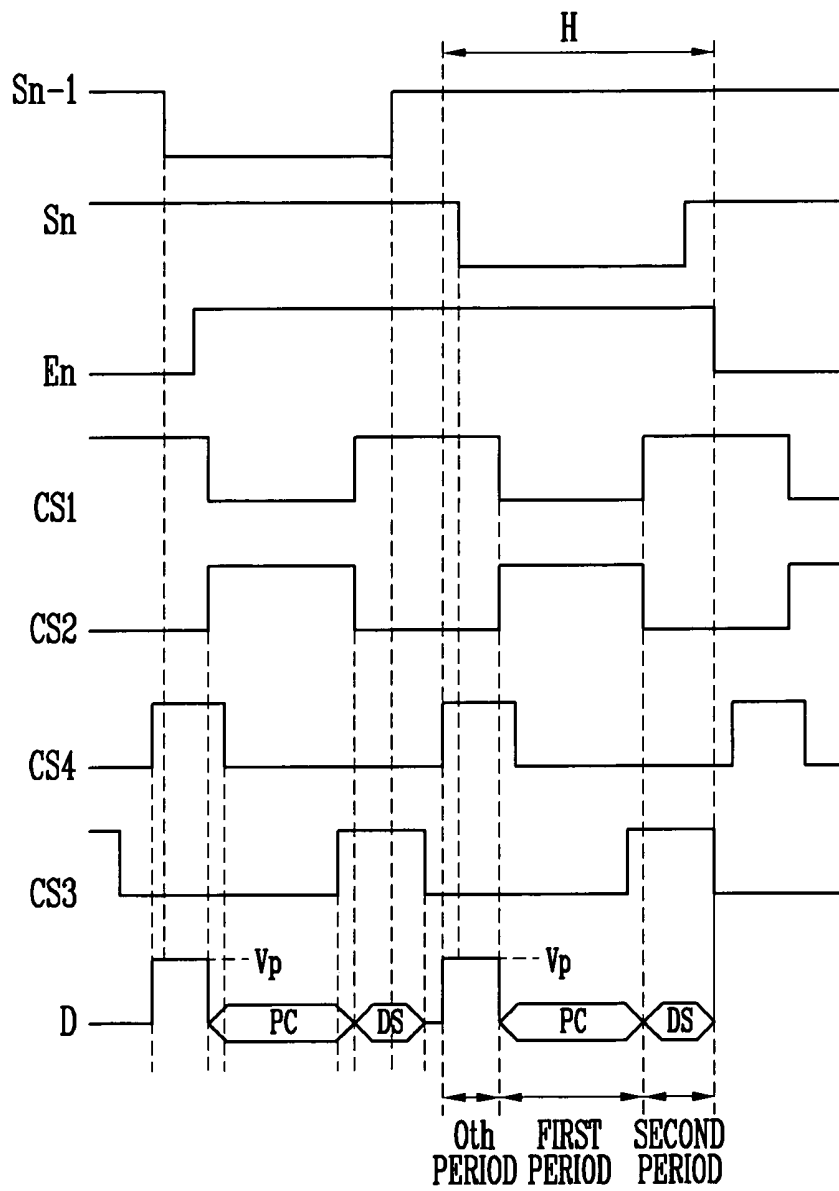


FIG. 14



DATA DRIVER, ORGANIC LIGHT EMITTING DISPLAY DEVICE USING THE SAME, AND METHOD OF DRIVING THE ORGANIC LIGHT EMITTING DISPLAY DEVICE

CROSS-REFERENCE TO RELATED APPLICATIONS

This application claims priority to and the benefit of Korean Patent Applications No. 10-2005-0073047 and No. 10-2005-0073048, filed on Aug. 10, 2005, in the Korean Intellectual Property Office, the entire content of both of which is incorporated herein by reference.

BACKGROUND

1. Field of the Invention

The present invention relates to a data driver, an organic light emitting display device using the same, and a method of driving the organic light emitting display device, and more particularly to, a data driver capable of displaying images with a substantially uniform brightness, an organic light emitting display device using the same, and a method of driving the organic light emitting display device.

2. Discussion of Related Art

Recently, various types of flat panel displays (FPDs) have been developed that reduced weight and volume compared to cathode ray tubes (CRT). The FPDs include liquid crystal displays (LCDs), field emission displays (FEDs), plasma display panels (PDPs), and organic light emitting display devices.

Among the FPDs, the organic light emitting display devices display images using organic light emitting diode devices that generate light by re-combination of electrons and holes. The organic light emitting display device has high response speed and is driven with low power consumption.

FIG. 1 illustrates the structure of a conventional organic light emitting display device.

Referring to FIG. 1, the conventional organic light emitting display device includes a display region 30 including a plurality of pixels 40 coupled to scan lines S1 to Sn and data lines D1 to Dm, a scan driver 10 for driving the scan lines S1 to Sn, a data driver 20 for driving the data lines D1 to Dm, and a timing controller 50 for controlling the scan driver 10 and the data driver 20.

The timing controller 50 generates data driving control signals DCS and scan driving control signals SCS in response to synchronizing signals supplied from the outside. The data driving control signals DCS generated by the timing controller 50 are supplied to the data driver 20 and the scan driving control signals SCS generated by the timing controller 50 are supplied to the scan driver 10. The timing controller 50 supplies the data Data supplied from the outside to the data driver 20.

The scan driver 10 receives the scan driving control signals SCS from the timing controller 50. The scan driver 10 then generates the scan signals to sequentially supply the generated scan signals to the scan lines S1 to Sn.

The data driver 20 receives the data driving control signals DCS from the timing controller 50. The data driver 20 then generates data signals and supplies the generated data signals to the data lines D1 to Dm in synchronization with the scan signals.

The display region 30 receives first and second power from a first power source ELVDD and a second power source ELVSS from the outside, respectively, and supplies the first and second power to the pixels 40. The pixels 40 then control

the currents that flow from the first power source ELVDD to the second power source ELVSS via an organic light emitting diode devices in response to the data signals to generate light components corresponding to the data signals.

That is, according to the conventional organic light emitting display device, each of the pixels 40 generates light with predetermined brightness in response to each of the data signals. However, according to the conventional organic light emitting display device, due to non-uniformity in the threshold voltages of transistors included in the pixels 40 and deviation in electron mobility, it may not be possible to display images with desired brightness. While the threshold voltages of the transistors included in the pixels 40 may be compensated for by controlling the structure of the pixel circuits included in the pixels 40, the deviation in the electron mobility is not compensated for. Therefore, an organic light emitting display device capable of displaying images with a substantially uniform brightness regardless of the deviation in the electron mobility is desired.

SUMMARY OF THE INVENTION

Accordingly, it is an aspect of the present invention to provide a data driver for driving an organic light emitting display device capable of displaying images with a substantially uniform brightness, an organic light emitting display device using the same, and a method of driving the organic light emitting display device.

In order to achieve the foregoing and/or other aspects of the present invention, according to a first embodiment of the present invention, there is provided a data driver for use in an organic light emitting display device that comprises a plurality of current sink units for performing control so that predetermined currents flow through data lines, a plurality of voltage generators for resetting the values of gray scale voltages using compensation voltages generated when the predetermined currents flow, a plurality of digital-to-analog converters for selecting one gray scale voltage among the gray scale voltages as a data signal in response to the bit values of the data supplied from the outside, and a plurality of switching units for supplying the data signal to the data lines.

The current sink units may receive the predetermined currents from pixels coupled to the data lines. The current sink units receive the predetermined currents in a first period that is a part of a horizontal period. The values of the predetermined currents are the same as the values of the currents that flow when the pixels emit light with the maximum brightness.

According to a second embodiment of the present invention, there is provided a data driver for driving an organic light emitting display device. The data driver includes a precharging unit for supplying a precharging voltage to a pixel coupled to a data line, a current sink unit receiving a predetermined current from the pixel, a voltage generator for resetting the values of gray scale voltages using a compensation voltage generated when the predetermined current flows, a digital-to-analog converter for selecting one gray scale voltage among the values of the gray scale voltages as a data signal in response to the bit value of the data supplied from the outside to the data driver, and a switching unit for supplying the data signal to the data line.

The precharging unit may be located between the digital-to-analog converter and the switching unit.

According to a third embodiment of the present invention, there is provided a method of driving an organic light emitting display device, the method comprising of (a) controlling predetermined currents to flow in data lines coupled to pixels, (b) generating compensation voltages corresponding to the pre-

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determined currents, (c) resetting the values of gray scale voltages using the compensation voltages, and (d) selecting one voltage among the gray scale voltages to correspond to the bit values of the data supplied from the outside to supply the selected voltage to the data line.

According to a fourth embodiment of the present invention, there is provided a method of driving an organic light emitting display device, the method comprising of supplying a predetermined precharging voltage to a pixel selected by a scan signal, supplying a predetermined current from the pixel to which the precharging voltage is supplied to a data driver, resetting the values of gray scale voltages using compensation voltages generated when the predetermined current is supplied, and selecting one of the gray scale voltages as a data signal to correspond to the bit values of the data supplied from the outside to supply the data signal to the pixel.

BRIEF DESCRIPTION OF THE DRAWINGS

These and/or other aspects and features of the invention will become apparent and more readily appreciated from the following description of the exemplary embodiments, taken in conjunction with the accompanying drawings of which:

FIG. 1 illustrates a conventional organic light emitting display device;

FIG. 2 illustrates an organic light emitting display device according to an embodiment of the present invention;

FIG. 3 is a circuit diagram illustrating an example of a pixel illustrated in FIG. 2;

FIG. 4 illustrates waveforms that describe a method of driving the pixel illustrated in FIG. 3;

FIG. 5 is a circuit diagram illustrating another example of the pixel illustrated in FIG. 2;

FIG. 6 is a block diagram illustrating an example of the data driver illustrated in FIG. 2;

FIG. 7 is a block diagram illustrating another example of the data driver illustrated in FIG. 2;

FIG. 8 illustrates an example of a connection among a voltage generator, a digital-to-analog converter, a first buffer, a second buffer, a switching unit, a current sink unit, and a pixel;

FIG. 9 illustrates a method of driving the pixel, the switching unit, and the current sink unit illustrated in FIG. 8;

FIG. 10 illustrates another example of the switching unit illustrated in FIG. 8;

FIG. 11 illustrates another example of the connection among the voltage generator, the digital-to-analog converter, the first buffer, the second buffer, the switching unit, the current sink unit, and the pixel;

FIG. 12 illustrates still another example of the data driver illustrated in FIG. 2;

FIG. 13 illustrates the connection among the voltage generator, the digital-to-analog converter, the first buffer, the second buffer, the switching unit, the current sink unit, and the pixel illustrated in FIG. 12; and

FIG. 14 illustrates waveforms that describe a method of driving the voltage generator, the switching unit, and the current sink unit illustrated in FIG. 13.

DETAILED DESCRIPTION

Hereinafter, exemplary embodiments of the present invention will be described with reference to FIGS. 2 to 14.

FIG. 2 illustrates an organic light emitting display device according to an embodiment of the present invention.

Referring to FIG. 2, the organic light emitting display device according to one embodiment of the present invention

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includes a display region 130 including a plurality of pixels 140 coupled to scan lines S1 to Sn, emission control lines E1 to En, and data lines D1 to Dm, a scan driver 110 for driving the scan lines S1 to Sn and the emission control lines E1 to En, a data driving part 120 for driving the data lines D1 to Dm, and a timing controller 150 for controlling the scan driver 110 and the data driving part 120.

The display region 130 includes the pixels 140 formed in the regions partitioned by the scan lines S1 to Sn, the emission control lines E1 to En, and the data lines D1 to Dm. The pixels 140 receive a first voltage from a first power source ELVDD, a second voltage from a second power source ELVSS, and a reference voltage from a reference power source Vref from the outside. The pixels 140 then compensate for drop of the voltage of the first power source ELVDD using a difference between the reference voltage of the reference power source Vref and the first voltage of the first power source ELVDD. The pixels 140 supply predetermined currents from the first power source ELVDD to the second power source ELVSS via organic light emitting diode devices (not shown) in response to data signals. Each of the pixels 140 may have the structure illustrated in FIG. 3 or 5. Detailed description of the structure of the pixel 140 illustrated in FIG. 3 or 5 will follow.

The timing controller 150 generates data driving control signals DCS and scan driving control signals SCS in response to synchronizing signals supplied from the outside. The data driving control signals DCS generated by the timing controller 150 are supplied to the data driving part 120 and the scan driving control signals SCS generated by the timing controller 150 are supplied to the scan driver 110. The timing controller 150 supplies data Data supplied from the outside to the data driving part 120.

The scan driver 110 receives the scan driving control signals SCS. The scan driver 110 then sequentially supplies scan signals to the scan lines S1 to Sn. The scan driver 110 also sequentially supplies emission control signals to the emission control lines E1 to En. Each of the emission control signals is supplied to overlap two scan signals. Therefore, a width of the emission control signals is equal to or larger than a width of the scan signals.

The data driving part 120 receives the data driving control signals DCS from the timing controller 150. The data driving part 120 then generates the data signals to be supplied to the data lines D1 to Dm. The data driving part 120 supplies predetermined currents to the data lines D1 to Dm in a first period of a horizontal period H and supplies predetermined voltages (representing the data signals) to the data lines D1 to Dm in a second period following the first period of the horizontal period H. Therefore, the data driving part 120 includes at least one data driver 200.

FIG. 3 illustrates pixel 1401 which is an example of the pixel 140 illustrated in FIG. 2. In FIG. 3, for the sake of convenience, the pixel coupled to the mth data line Dm, the (n-1)th and nth scan lines Sn-1 and Sn, and the nth emission control line En is illustrated.

Referring to FIG. 3, the pixel 1401 in one embodiment of the present invention includes an organic light emitting diode (OLED) and a pixel circuit 1421 for supplying current to the OLED.

The OLED generates light of a predetermined color in response to the current supplied from the pixel circuit 1421.

The pixel circuit 1421 compensates for drop in the first voltage from the first power source ELVDD and a threshold voltage of a fourth transistor M4 when a scan signal is supplied to the (n-1)th scan line Sn-1 (the previous scan line) and charges the voltage corresponding to the data signal when the scan signal is supplied to the nth scan line Sn (the current

or the present scan line). Therefore, the pixel circuit 1421 includes first, second, third, fourth, fifth, sixth transistors M1, M2, M3, M4, M5, and M6, a first capacitor C1, and a second capacitor C2. Each transistor has first and second electrodes and a gate electrode.

The first electrode of the first transistor M1 is coupled to the data line Dm and the second electrode of the first transistor M1 is coupled to a first node N1. The gate electrode of the first transistor M1 is coupled to the nth scan line Sn. The first transistor M1 is turned on when the scan signal is supplied to the nth scan line Sn to electrically connect the data line Dm and the first node N1 to each other.

The first electrode of the second transistor M2 is coupled to the data line Dm and the second electrode of the second transistor M2 is coupled to the second electrode of the fourth transistor M4. The gate electrode of the second transistor M2 is coupled to the nth scan line Sn. The second transistor M2 is turned on when the scan signal is supplied to the nth scan line Sn to electrically connect the data line Dm and the second electrode of the fourth transistor M4 to each other.

The first electrode of the third transistor M3 is coupled to the reference power source Vref and the second electrode of the third transistor M3 is coupled to the first node N1. The gate electrode of the third transistor M3 is coupled to the (n-1)th scan line Sn-1. The third transistor M3 is turned on when the scan signal is supplied to the (n-1)th scan line Sn-1 to electrically connect the reference power source Vref and the first node N1 to each other.

The first electrode of the fourth transistor M4 is coupled to the first power source ELVDD and the second electrode of the fourth transistor M4 is coupled to the first electrode of the sixth transistor M6. The gate electrode of the fourth transistor M4 is coupled to a second node N2. The fourth transistor M4 supplies the current corresponding to the voltage applied to the second node N2, that is, the voltage charged in the first and second capacitors C1 and C2, to the first electrode of the sixth transistor M6.

The second electrode of the fifth transistor M5 is coupled to the second node N2 and the first electrode of the fifth transistor M5 is coupled to the second electrode of the fourth transistor M4. The gate electrode of the fifth transistor M5 is coupled to the (n-1)th scan line Sn-1. The fifth transistor M5 is turned on when the scan signal is supplied to the (n-1)th scan line Sn-1 so that current flows through the fourth transistor M4 and that the fourth transistor M4 operates as a diode.

The first electrode of the sixth transistor M6 is coupled to the second electrode of the fourth transistor M4 and the second electrode of the sixth transistor M6 is coupled to the anode electrode of the OLED. The gate electrode of the sixth transistor M6 is coupled to the nth emission control line En. The sixth transistor M6 is turned off when an emission control signal is supplied to the nth emission control line En and is turned on when no emission control signal is supplied. Here, the emission control signal supplied to the nth emission control line En is supplied to overlap the scan signals supplied to the (n-1)th scan line Sn-1 and the nth scan line Sn. Therefore, the sixth transistor M6 is turned off when the scan signal is supplied to the (n-1)th scan line Sn-1 and the nth scan line Sn so that predetermined voltage is charged in the first and second capacitors C1 and C2 and is turned on in the other cases to electrically connect the fourth transistor M4 and the OLED to each other. While in FIG. 3, for the sake of convenience, the transistors M1 to M6 are shown as PMOS transistors, the present invention is not limited to a circuit including PMOS transistors.

In the pixel 1401 illustrated in FIG. 3, the reference power source Vref does not supply current to the OLED. Since the reference power source Vref does not supply current to the pixel 1401, a drop in voltage is not generated. Therefore, it is possible to maintain the voltage value of the reference power source Vref uniform regardless of the positions of the pixels 140. The voltage value of the reference power source Vref may be equal to or different from the voltage of the first power source ELVDD.

FIG. 4 illustrates waveforms that describe a method of driving the pixel illustrated in FIG. 3. In FIG. 4, a horizontal period H is divided into a first period and a second period to be driven. In the first period, a predetermined current (PC) flows to the data lines D1 to Dm. In the second period, a data signal DS is supplied to the data lines D1 to Dm. The PC is supplied from the pixel 1401 to one of the data drivers 200 which operates as a current sink.

The data signal DS is supplied from the data driver 200 to the pixel 1401. Hereinafter, for the sake of convenience, it is assumed that the initial voltage value of the reference power source Vref is equal to the initial voltage value of the first power source ELVDD.

Operation processes will be described in detail with reference to FIGS. 3 and 4. First, the scan signal is supplied to the (n-1)th scan line Sn-1. When the scan signal is supplied to the (n-1)th scan line Sn-1, the third and fifth transistors M3 and M5 are turned on. When the fifth transistor M5 is turned on, current flows through the fourth transistor M4 and the fourth transistor M4 operates as a diode. When the fourth transistor M4 operates as a diode, the voltage value obtained by subtracting the threshold voltage of the fourth transistor M4 from the first power source ELVDD is applied to the second node N2.

When the third transistor M3 is turned on, the voltage of the reference power source Vref is applied to the first node N1. At this time, the second capacitor C2 is charged with the voltage corresponding to difference between the first node N1 and the second node N2. In this case, when it is assumed that the reference power source Vref is equal to the voltage value of the first power source ELVDD, the voltage corresponding to the threshold voltage of the fourth transistor M4 is charged in the second capacitor C2. When predetermined drop in voltage is generated in the first power source ELVDD, the threshold voltage of the fourth transistor M4 and the voltage corresponding to the voltage drop of the first power source ELVDD are charged in the second capacitor C2. That is, according to the present invention, in the period where the scan signal is supplied to the (n-1)th scan line Sn-1, the voltage corresponding to the voltage drop of the first power source ELVDD and the threshold voltage of the fourth transistor M4 are charged in the second capacitor C2. Accordingly, it is possible to compensate for the voltage drop of the first power source ELVDD.

After a predetermined voltage is charged in the second capacitor C2, the scan signal is supplied to the nth scan line Sn. When the scan signal is supplied to the nth scan line Sn, the first and second transistors M1 and M2 are turned on. When the second transistor M2 is turned on, in the first period of the horizontal period H, the PC is supplied from the pixel 1401 to the data driver 200 via the data line Dm. In more detail, the PC is supplied to the data driver 200 via the first power source ELVDD, the fourth transistor M4, the second transistor M2, and the data line Dm. At this time, a predetermined voltage is charged in the first and second capacitors C1 and C2 in response to the PC.

On the other hand, the data driver 200 resets the voltage of a gamma voltage unit (not shown) using a compensation

voltage generated when the PC sinks to generate the data signal DS using the reset voltage of the gamma voltage unit. Then, the data signal DS is supplied to the first node N1 via the first transistor M1 in the second period of the horizontal period H. Then, the voltage corresponding to a difference between the data signal DS and the voltage of the first power source ELVDD is charged in the first capacitor C1. At this time, since the second node N2 floats, the second capacitor C2 maintains the previously charged voltage.

That is, according to the described embodiment of the present invention, in the period where the scan signal is supplied to one of the scan lines, called a previous scan line (i.e., Sn-1), the threshold voltage of the fourth transistor M4 and the voltage corresponding to the voltage drop of the first power source ELVDD are charged in the second capacitor C2 so that it is possible to compensate for the voltage drop of the first power source ELVDD and the threshold voltage of the fourth transistor M4. According to the described embodiment of the present invention, the voltage of the gamma voltage unit is reset so that the electron mobility of the transistors included in the pixel 1401 is compensated for during the period in which the scan signal is supplied to the next scan line, called a current or a present scan line (i.e., Sn), and the generated data signal is supplied using the reset gamma voltage. Therefore, according to the described embodiment of the present invention, non-uniformity in the threshold voltages of the transistors and the electron mobility is compensated for, so that it is possible to display images with a substantially uniform brightness. Processes of resetting the voltage of the gamma voltage unit will be described later.

FIG. 5 illustrates a pixel 1402 which is another example of the pixel 140 illustrated in FIG. 2. The pixel 1402 includes a pixel circuit 1422 that includes first, second, third, fourth, fifth, and sixth transistors M1', M2', M3', M4', M5', and M6', a first capacitor C1', and a second capacitor C2'. Each transistor has first and second electrodes and a gate electrode. The structure of the pixel 1402 illustrated in FIG. 5 is the same as the structure of the pixel 1401 illustrated in FIG. 3 except that the first capacitor C1' is now provided between the second node N2' and the first power source ELVDD.

Operation processes will be described in detail with reference to FIGS. 4 and 5. First, the scan signal is supplied to the (n-1)th scan line Sn-1. When the scan signal is supplied to the (n-1)th scan line Sn-1, the third and fifth transistors M3' and M5' are turned on. When the fifth transistor M5' is turned on, current flows through the fourth transistor M4' so that the fourth transistor M4' operates as a diode. When the fourth transistor M4' operates as a diode, the voltage value obtained by subtracting the threshold voltage of the fourth transistor M4' from the first power source ELVDD is applied to the second node N2'. Therefore, the voltage corresponding to the threshold voltage of the fourth transistor M4' is charged in the first capacitor C1'.

When the third transistor M3' is turned on, the voltage of the reference power source Vref is applied to the first node N1'. Then, the second capacitor C2' charges the voltage corresponding to a difference between the first node N1' and the second node N2'. Here, since the first and second transistors M1' and M2' are turned off in the period where the scan signal is supplied to the (n-1)th scan line Sn-1, the data signal DS is not supplied to the pixel 1402.

Then, the scan signal is supplied to the nth scan line Sn so that the first and second transistors M1' and M2' are turned on. When the second transistor M2' is turned on, in the first period of the horizontal period H, the PC is supplied from the pixel 1402 to the data driver 200 via the data line Dm. Actually, the PC is supplied to the data driver 200 via the first power source

ELVDD, the fourth transistor M4', the second transistor M2', and the data line Dm. At this time, a predetermined voltage is charged in the first and second capacitors C1' and C2' in response to a first data signal DS1.

The data driver 200 resets the voltage of the gamma voltage unit (not shown) using the compensation voltage applied in response to the PC to generate the data signal DS using the reset voltage of the gamma voltage unit. Then, in the second period of the horizontal period H, the data signal DS is supplied to the first node N1'. Then, the predetermined voltage corresponding to the data signal DS is charged in the first and second capacitors C1' and C2'.

Actually, when the data signal DS is supplied, the voltage of the first node N1' falls from the voltage of the reference power source Vref to the voltage of the data signal DS. Since the second node N2' floats, the voltage at the second node N2' is reduced in response to the amount of voltage drop of the first node N1'. The amount of reduction in the voltage of the second node N2' is determined by the capacitance values of the first and second capacitors C1' and C2'.

When the voltage of the second node N2' falls, the predetermined voltage corresponding to the voltage value of the second node N2' is charged in the first capacitor C1'. Here, since the voltage value of the reference power source Vref is fixed, the voltage charged in the first capacitor C1' is determined by the data signal DS. That is, since the voltage values charged in the capacitors C1' and C2' are determined by the reference power source Vref and the data signal DS in the pixel 1402 illustrated in FIG. 5, it is possible to charge a desired voltage regardless of the voltage drop of the first power source ELVDD.

According to the described embodiments of the present invention, the voltage of the gamma voltage unit is reset to compensate for the electron mobility of the transistors included in the pixel 1402 and to supply the generated data signal using the reset gamma voltage. Therefore, according to the described embodiments of the present invention, non-uniformity in the threshold voltages of the transistors and deviation in the electron mobility of the transistors is compensated for so that it is possible to display images with a substantially uniform brightness.

FIG. 6 is a block diagram illustrating an exemplary embodiment of a data driver 201, which is an example of the data driver 200 illustrated in FIG. 2. In FIG. 6, for the sake of convenience, it is assumed that the data driver 201 has j (j is a natural number not less than 2) channels.

Referring to FIG. 6, the data driver 201 according to the embodiment of the present invention includes a shift register unit 210, a sampling latch unit 220, a holding latch unit 230, a gamma voltage unit 240, a digital-to-analog converter unit (hereinafter, referred to as a DAC) 250, a first buffer unit 270, a second buffer unit 260, a current supplying unit 280, and a selector 290.

The shift register unit 210 receives a source shift clock SSC and a source start pulse SSP from the timing controller 150. The shift register unit 210 then sequentially generates j sampling signals while shifting the source start pulse SSP every one period of the source shift clock SSC. Therefore, the shift register unit 210 includes j shift registers 2101 to 210j.

The sampling latch unit 220 sequentially stores the data Data in response to the sampling signals sequentially supplied from the shift register unit 210. Here, the sampling latch unit 220 includes j sampling latches 2201 to 220j in order to store the j data Data. Each of the sampling latches 2201 to 220j has the magnitude corresponding to the number of bits of

the data Data. For example, when the data Data is composed of k bits, each of the sampling latches 2201 to 220j has the magnitude of k bits.

The holding latch unit 230 receives the data Data from the sampling latch unit 220 to store the data Data when a source output enable signal SOE is input. The holding latch unit 230 supplies the data Data stored therein to the DAC unit 250, when the source output enable signal SOE is input. Here, the holding latch unit 230 includes j holding latches 2301 to 230j in order to store the j data Data. Each of the holding latches 2301 to 230j has the magnitude corresponding to the number of bits of the data Data. For example, each of the holding latches 2301 to 230j has the magnitude of k bits to store the data Data.

The gamma voltage unit 240 includes j voltage generators 2401 to 240j for generating predetermined gray scale voltage in response to the data Data of k bits. As illustrated in FIG. 8, each of the voltage generators 2401 to 240j is composed of a plurality of voltage dividing resistors R(1) to R(l) to generate 2^k gray scale voltages. Here, the voltage generators 2401 to 240j reset the values of the gray scale voltages using the compensation voltage supplied from the second buffer unit 260 to supply the reset gray scale voltages to the DACs 2501 to 250j.

The DAC unit 250 includes j DACs 2501 to 250j that generate the data signal DS in response to the bit values of the data Data. Each of the DACs 2501 to 250j selects one of the plurality of gray scale voltages in response to the bit values of the data Data supplied from the holding latch unit 230 to generate a second data signal DS2.

The first buffer unit 270 supplies the data signals DS supplied from the DAC unit 250 to the selector 290. Therefore, the first buffer unit 270 includes j first buffers 2701 to 270j.

The selector 290 controls electrical connection between the data lines D1 to Dj and the first buffers 2701 to 270j. Actually, the selector 290 electrically connects the data lines D1 to Dj and the first buffers 2701 to 270j to each other only in the second period of the horizontal period H and does not connect the data lines D1 to Dj and the first buffers 2701 to 270j to each other in the other period. Therefore, the selector 290 includes j switching units 2901 to 290j.

The current supplying unit 280 sinks the PC from the pixels 140 coupled to the data lines D1 to Dj in the first period of the horizontal period H. Actually, the current supplying unit 280 sinks the maximum current that can flow through each of the pixels 140, that is, the current to be supplied to the OLED when the pixel 140 emits light with the maximum brightness. The current supplying unit 280 supplies a predetermined compensation voltage generated when the current sinks to the second buffer unit 260. Therefore, the current supplying unit 280 includes j current sink units 2801 to 280j.

The second buffer unit 260 supplies the compensation voltage supplied from the current supplying unit 280 to the gamma voltage unit 240. Therefore, the second buffer unit 260 includes j second buffers 2601 to 260j.

On the other hand, as illustrated in FIG. 7, a data driver 202, which is an example of the data driver 200 according to one exemplary embodiment of the present invention may further include a level shifter unit 310 after the holding latch unit 230. The level shifter unit 310 increases the voltage levels of the data Data supplied from the holding latch unit 230 to supply the data Data to the DAC unit 250. When the data Data having a high voltage level are supplied from an external system to the data driver 200, circuit parts having a high voltage resistant property must be provided in response to the voltage level so that manufacturing cost increases. Therefore, the data Data having a low voltage level are supplied from the outside of the

data driver 200 and the low voltage level is transited to a high voltage level by the level shifter unit 310.

FIG. 8 illustrates a connection among the voltage generator, the DAC, the first buffer, the second buffer, the switching unit, the current sink unit, and the pixel circuit provided in a specific channel. In FIG. 8, for the sake of convenience, a jth channel is illustrated and it is assumed that the data line Dj is coupled to the pixel circuit 1421 of the pixel 1401 illustrated in FIG. 3.

Referring to FIG. 8, the voltage generator 240j includes a plurality of voltage dividing resistors R(1) to R(l). The voltage dividing resistors R(1) to R(l) are positioned between the reference power source Vref and the second buffer 260j. The voltage dividing resistors R(1) to R(l) divide the voltage between the voltage of the reference power source Vref and the compensation voltage supplied from the second buffer 260j to generate a plurality of gray scale voltages to V(0) to V(2^k-1) and to supply the generated gray scale voltages to the DAC 250j.

The DAC 250j selects one gray scale voltage among the gray scale voltages V(0) to V(2^k-1) in response to the bit values of the data Data to supply the selected gray scale voltage to the first buffer 270j. Here, the gray scale voltage selected by the DAC 250j is used as the data signal DS.

The first buffer 270j transmits the data signal DS supplied from the DAC 250j to the switching unit 290j.

The switching unit 290j includes an 11th transistor M11. The 11th transistor M11 is controlled by the first control signal CS1 illustrated in FIG. 9. That is, the 11th transistor M11 is turned on in the second period of the horizontal period H and is turned off in the first period. Therefore, the data signal DS is supplied to the data line Dj in the second period of the horizontal period H and is not supplied in the other period.

The current sink unit 280j includes 12th and 13th transistors M12 and M13 controlled by the second control signal CS2, a current source I_{max} coupled to the first electrode of the 13th transistor M13, and a third capacitor C3 coupled between a third node N3 and a ground voltage source GND. The 12th and 13th transistors M12 and M13 each have a gate electrode and first and second electrodes.

The gate electrode of the 12th transistor M12 is coupled to the gate electrode of the 13th transistor M13 and the second electrode of the 12th transistor M12 is coupled to the second electrode of the 13th transistor M13 and the data line Dj. The first electrode of the 12th transistor M12 is coupled to the second buffer 260j. The 12th transistor M12 is turned on in the first period of the horizontal period H by the second control signal CS2 and is turned off in the second period.

The first electrode of the 13th transistor M13 is coupled to the current source I_{max}. The 13th transistor M13 is also turned on by the second control signal CS2 in the first period of the horizontal period H and is turned off in the second period.

The current source I_{max} receives the current to be supplied to the OLED when the pixel 1401 emits light with a maximum brightness in the first period where the 12th and 13th transistors M12 and M13 are turned on.

The third capacitor C3 stores the compensation voltage applied to the third node N3 when the current source I_{max} operates as a current sink for the current from the pixel 1401. The third capacitor C3 that has been charged with the compensation voltage in the first period, maintains the compensation voltage of the third node N3 uniform even when the 12th and 13th transistors M12 and M13 are turned off in the second period.

The second buffer 260j transmits the compensation voltage applied to the third node N3, that is, the voltage charged in the

third capacitor C3 to the voltage generator 240j. Then, the voltage generator 240j divides the voltage between the voltage of the reference power source Vref and the compensation voltage supplied from the second buffer 260j. Here, the compensation voltage applied to the third node N3 is set to be the same or to vary in each pixel 140 in accordance with the electron mobility of the transistors included in the pixel 140. The compensation voltage supplied to the j voltage generators 2401 to 240j is determined by the currently coupled pixel 140.

On the other hand, when different compensation voltages are supplied to the j voltage generators 2401 to 240j, the values of the gray scale voltages V(0) to V(2^k-1) supplied to the DACs 2501 to 250j provided in the j channels are set to be different from each other. Here, since the gray scale voltages V(0) to V(2^k-1) are controlled by the pixels 140 to which the data lines D1 to Dj are currently coupled, although the electron mobility of the transistors included in the pixels 140 is non-uniform, the display region 130 can display images with a substantially uniform brightness.

FIG. 9 illustrates driving waveforms supplied to the switching unit, the current sink unit, and the pixel illustrated in FIG. 8.

The voltage value of the data signal DS supplied to the pixel 140 will be described in detail with reference to FIGS. 8 and 9. First, the scan signal is supplied to the (n-1)th scan line Sn-1. When the scan signal is supplied to the (n-1)th scan line Sn-1, the third and fifth transistors M3 and M5 are turned on. Then, the voltage value obtained by subtracting the threshold voltage of the fourth transistor M4 from the first power source ELVDD is applied to the second node N2 and the voltage of the reference power source Vref is applied to the first node N1. At this time, the voltage corresponding to the voltage drop of the first power source ELVDD and the threshold voltage of the fourth transistor M4 are charged in the second capacitor C2.

Actually, the voltages applied to the first node N1 and the second node N2 are represented by EQUATION 1.

$$V_{N1} = V_{ref}$$

$$V_{N2} = ELVDD - |V_{thM4}| \quad \text{[EQUATION 1]}$$

wherein, V_{N1}, V_{N2}, and V_{thM4} represent the voltage applied to the first node N1, the voltage applied to the second node N2, and the threshold voltage of the fourth transistor M4, respectively.

On the other hand, in a period between the point of time when the scan signal supplied to the (n-1)th scan line Sn-1 is turned off and the point of time when the scan signal is supplied to the nth scan line Sn, the first and second nodes N1 and N2 float. Therefore, the voltage value charged in the second capacitor C2 does not change.

Then, the scan signal is supplied to the nth scan line Sn so that the first and second transistors M1 and M2 are turned on. While the scan signal is supplied to the nth scan line Sn, in the first period, the 12th and 13th transistors M12 and M13 are also turned on. When the 12th and 13th transistors M12 and M13 are turned on, a current flows through the current source I_{max} via the first power source ELVDD, the fourth transistor M4, the second transistor M2, the data line Dj, and the 13th transistor M13 and the current source I_{max} operates as a current sink for this current.

At this time, since the current of the current source I_{max} flows through the fourth transistor M4, EQUATION 2 is obtained.

$$I_{max} = \frac{1}{2} \mu_p C_{ox} \frac{W}{L} (ELVDD - V_{N2} - |V_{thM4}|)^2 \quad \text{[EQUATION 2]}$$

wherein, μ, Cox, W, and L represent electron mobility, the capacity of an oxide layer, the width of a channel, and the length of a channel, of the fourth transistor M4, respectively.

The voltage applied to the second node N2 when the current obtained by EQUATION 2 flows through the fourth transistor M4 may be represented by EQUATION 3.

$$V_{N2} = ELVDD - \sqrt{\frac{2I_{max} L}{\mu_p C_{ox} W}} - |V_{thM4}| \quad \text{[EQUATION 3]}$$

The voltage applied to the first node N1 may be represented by EQUATION 4 by the coupling of the second capacitor C2.

$$V_{N1} = V_{ref} - \sqrt{\frac{2I_{max} L}{\mu_p C_{ox} W}} = V_{N3} = V_{N4} \quad \text{[EQUATION 4]}$$

wherein, the voltage V_{N1} applied to the first node N1 may be equal to the voltage V_{N3} applied to the third node N3 and the voltage V_{N4} applied to a fourth node N4 formed between the second buffer 260j and the voltage generator 240j. That is, when the current is sunk by the current source I_{max}, the voltage obtained by EQUATION 4 is applied to the fourth node N4.

However, as illustrated by EQUATION 4, the voltage applied to the third node N3 and the fourth node N4 is affected by the electron mobility of the transistors included in the pixel 140 the current from which sinks into the current source I_{max}. Therefore, the value of the voltage applied at the third node N3 and the fourth node N4 when the current is sunk by the current source I_{max} varies in each of the pixels 140 according to the electron mobility of each of the pixels 140.

When the voltage obtained by EQUATION 4 is applied to the fourth node N4, a voltage V_{diff} across the voltage generator 240j may be represented by EQUATION 5.

$$V_{diff} = V_{ref} - \left(V_{ref} - \sqrt{\frac{2I_{max} L}{\mu_p C_{ox} W}} \right) \quad \text{[EQUATION 5]}$$

When the DAC 250j selects the hth (h is a natural number) gray scale voltage among f (f is a natural number less than or equal to h) gray scale voltages in response to the data Data, the voltage Vb supplied to the first buffer 270j may be represented by EQUATION 6.

$$Vb = V_{ref} - \frac{h}{f} \sqrt{\frac{2I_{max} L}{\mu_p C_{ox} W}} \quad \text{[EQUATION 6]}$$

After the current sinks in the first period so that the voltage obtained by EQUATION 4 is charged in the third capacitor C3, the 12th and 13th transistors M12 and M13 are turned off in the second period and the 11th transistor M11 is turned on. At this time, the third capacitor C3 maintains the voltage value charged therein. Therefore, the voltage value of the third node N3 may be maintained as illustrated in EQUATION 4.

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Since the 11th transistor M11 is turned on in the second period, the voltage supplied to the first buffer 270j is supplied to the first node N1 via the 11th transistor M11, the data line Dj, and the first transistor M1. That is, the voltage obtained by EQUATION 6 is supplied to the first node N1. The voltage applied to the second node N2 by the coupling of the second capacitor C2 may be represented by EQUATION 7.

$$V_{N2} = ELVDD - \frac{h}{f} \sqrt{\frac{2I_{max}}{\mu_p C_{ox}} \frac{L}{W}} - |V_{thM4}| \quad \text{[EQUATION 7]}$$

At this time, the current that flows via the fourth transistor M4 may be represented by EQUATION 8.

$$\begin{aligned} I_{M4} &= \frac{1}{2} \mu_p C_{ox} \frac{W}{L} (ELVDD - V_{N2} - |V_{thM4}|)^2 \\ &= \frac{1}{2} \mu_p C_{ox} \frac{W}{L} \left(ELVDD - \left(ELVDD - \frac{h}{f} \sqrt{\frac{2I_{max}}{\mu_p C_{ox}} \frac{L}{W}} - |V_{thM4}| \right) - V_{thM4} \right)^2 \\ &= \left(\frac{h}{f} \right)^2 I_{max} \end{aligned} \quad \text{[EQUATION 8]}$$

Referring to EQUATION 8, according to the present invention, the current that flows through the fourth transistor M4 is determined by the gray scale voltage generated by the voltage generator 240j. That is, according to the present invention, the current determined by the gray scale voltage can flow to the fourth transistor M4 regardless of the threshold voltage and electron mobility of the fourth transistor M4. Therefore, it is possible to display images with a substantially uniform brightness.

On the other hand, according to the present invention, the structure of the switching unit 290j may vary. For example, in the switching unit 290j, as illustrated in FIG. 10, the 11th transistor M11 and a 14th transistor M14 may be coupled to each other in the form of a transmission gate. The 14th transistor M14 formed of PMOS receives a second control signal CS2. The 11th transistor M11 formed of NMOS receives the first control signal CS1. As shown in FIG. 9, since the polarity of the first control signal CS1 is opposite to the polarity of the second control signal CS2, the 11th and 14th transistors M11 and M14 are turned on and off at the same time.

On the other hand, when the 11th and 14th transistors M11 and M14 are coupled to each other in the form of the transmission gate, a voltage-current characteristic curve is in the form of a straight line so that it is possible to minimize switching error.

FIG. 11 illustrates another example of the connection among the voltage generator, the DAC, the first buffer, the second buffer, the switching unit, the current sink unit, and the pixel provided in the specific channel. The structure of FIG. 11 is the same as the structure of FIG. 8 except that the pixel 1402 is coupled to the data line Dj instead of the first exemplary pixel 1401. Therefore, the voltage supplied to the pixel 1402 will be simply described.

Referring to FIGS. 9 and 11, first, when the scan signal is supplied to the (n-1)th scan line Sn-1, the voltage obtained by EQUATION 1 is applied to the first and second nodes N1' and N2'.

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The current that flows through the fourth transistor M4' in the first period when the scan signal is supplied to the nth scan line Sn and the 12th and 13th transistors M12' and M13' are turned on is also represented by EQUATION 2 that pertained to the fourth transistor M4 of the first exemplary pixel circuit 1421 and the voltage applied to the second node N2' in the first period is also represented by EQUATION 3.

The voltage applied to the first node N1' by the coupling of the second capacitor C2' may be represented by EQUATION 9.

$$V_{N1'} = V_{ref} - \left(\frac{C1' + C2'}{C2'} \right) \sqrt{\frac{2I_{max}}{\mu_p C_{ox}} \frac{L}{W}} \quad \text{[EQUATION 9]}$$

$$= V_{N3'}$$

$$= V_{N4'}$$

Since the voltage applied to the first node N1' is also supplied to the third node N3 and the fourth node N4, the voltage V_{diff} across the voltage generator 240j may be represented by EQUATION 10.

$$V_{diff} = \quad \text{[EQUATION 10]}$$

$$V_{ref} - \left(V_{ref} - \left(\frac{C1' + C2'}{C2'} \right) \sqrt{\frac{2I_{max}}{\mu_p C_{ox}} \frac{L}{W}} \right)$$

When the DAC 250j selects the hth gray scale voltage among f gray scale voltages, the voltage Vb supplied to the first buffer 270j may be represented by EQUATION 11.

$$Vb = V_{ref} - \frac{h}{f} \left(\frac{C1' + C2'}{C2'} \right) \sqrt{\frac{2I_{max}}{\mu_p C_{ox}} \frac{L}{W}} \quad \text{[EQUATION 11]}$$

The voltage supplied to the first buffer 270j is supplied to the first node N1'. At this time, the voltage applied to the second node N2' may be represented also by EQUATION 7. Therefore, the current that flows through the fourth transistor M4' may be represented by EQUATION 8. That is, according to the present invention, the current supplied to the OLED via the fourth transistor M4' is determined by the gray scale voltage regardless of the threshold voltage and electron mobility of the fourth transistor M4'. Therefore, it is possible to display images with a substantially uniform brightness.

On the other hand, in the pixel 1402 illustrated in FIG. 5, the voltage of the second node N2' gradually changes although the voltage of the first node N1' rapidly changes because it changes proportionally to (C1'+C2')/C2'. Therefore, when the pixel 1402 illustrated in FIG. 5 is used, it is possible to set the voltage range of the voltage generator 240j larger than in the case where the pixel 1401 illustrated in FIG. 3 is applied. As described above, when the voltage range of the voltage generator 240j is set to be larger, it is possible to reduce the influence of the switching error of the 11th transistor M11' and the first transistor M1'.

FIG. 12 illustrates another example 203 of the data driver 200 illustrated in FIG. 2.

Referring to FIG. 12, the data driver 203 according to another embodiment of the present invention further includes a voltage supply unit 300 provided between the first buffer unit 270 and the DAC unit 250 when compared with the data driver 201 shown in FIG. 6.

The voltage supply unit **300** supplies a precharging voltage Vp to the first buffer unit **270** every horizontal period. Therefore, each horizontal period is divided into a 0th period, a first period, and a second period as illustrated in FIG. 14. Here, the voltage supply unit **300** supplies the precharging voltage Vp to the first buffer unit **270** in the 0th period of each horizontal period H. That is, the voltage supply unit **300** supplies the precharging voltage before the PC sinks into the current sink I_{max}. Therefore, it is possible to reduce the time required for sinking the PC.

The voltage supply unit **300** electrically connects the DAC unit **250** and the first buffer unit **270** to each other in the second period of each horizontal period H. Therefore, the voltage supply unit **300** includes j precharging units **3001** to **300j**.

The first buffer unit **270** supplies the precharging voltage supplied from the precharging units **3001** to **300j** and the data signals DS supplied from the DAC unit **250** to the switching unit **290j**.

The selector **290** controls electrical connection between the data lines D1 to Dj and the first buffers **2701** to **270j**. The selector **290** electrically couples the data lines D1 to Dj and the first buffers **2701** to **270j** to one another in the 0th period in which the precharging voltage Vp is supplied and in the second period in which the data signals DS are supplied and does not connect the data lines D1 to Dj and the first buffers **2701** to **270j** to each other in the first period.

FIG. 13 illustrates the connection among the voltage generator, the DAC unit, the precharging unit, the first buffer, the second buffer, the switching unit, the current sink unit, and the pixel provided in one specific channel of the data driver illustrated in FIG. 12.

Referring to FIG. 13, the voltage generator **240j** includes a plurality of voltage dividing resistors R(1) to R(l). The voltage dividing resistors R(1) to R(l) are provided between the reference power source V_{ref} and the second buffer **260j** to divide a voltage. Actually, the voltage dividing resistors R(1) to R(l) divide the voltage between the voltage of the reference power source V_{ref} and the compensation voltage supplied from the second buffer **260j** to generate the plurality of gray scale voltages V(0) to V(2^k-1) and to supply the generated gray scale voltages V(0) to V(2^k-1) to the DAC **250j**.

The DAC **250j** selects one gray scale voltage among the gray scale voltages V(0) to V(2^k-1) in response to the bit values of the data Data to supply the selected gray scale voltage to the precharging unit **300j**. Here, the gray scale voltage selected by the DAC **250j** is used as the data signal DS.

The precharging unit **300j** includes the 14th and 15th transistors M14 and M15. The 14th transistor M14 is provided between the DAC **250j** and the first buffer **270j** to be controlled by a third control signal CS3 illustrated in FIG. 14. The 14th transistor M14 is turned on in the second period of the horizontal period H to supply the data signal DS supplied from the DAC **250j** to the first buffer **270j**.

The 15th transistor M15 is provided between the precharging voltage source Vp and the first buffer **270j** to be controlled by the fourth control signal CS4. That is, the 15th transistor M15 is turned on in the 0th period of the horizontal period H to supply the precharging voltage Vp to the first buffer **270j**.

The first buffer **270j** transmits the precharging voltage Vp and the data signal DS supplied from the precharging unit **300j** to the switching unit **290j**.

The switching unit **290j** includes the 11th transistor M11. The 11th transistor M11 is controlled by the first control signal CS1. That is, the 11th transistor M11 is turned on in the 0th and

second periods of the horizontal period H to supply the precharging voltage Vp and the data signal DS to the data line Dj.

The current sink unit **280j** includes the 12th and 13th transistors M12 and M13 controlled by the second control signal CS2, the current source I_{max} coupled to the first electrode of the 13th transistor M13, and the third capacitor C3 coupled between the third node N3 and the ground voltage source GND.

The gate electrode of the 12th transistor M12 is coupled to the gate electrode of the 13th transistor M13. The second electrode of the 12th transistor M12 is coupled to the second electrode of the 13th transistor M13 and the data line Dj. The first electrode of the 12th transistor M12 is coupled to the second buffer **260j**. The 12th transistor M12 is turned on by the second control signal CS2 in the first period of the horizontal period H. The first electrode of the 13th transistor M13 is coupled to the current source I_{max}. The 13th transistor M13 is also turned on by the second control signal CS2 in the first period of the horizontal period H.

The current source I_{max} receives the current to be supplied to the OLED when the pixel **1401** emits light with the maximum brightness in the second period when the 12th and 13th transistors M12 and M13 are turned on.

The third capacitor C3 stores the compensation voltage applied to the third node N3 when the 12th and 13th transistors M12 and M13 are on and the current from the pixel **1401** is sunk by the current source I_{max} that is operating as a current sink. The third capacitor C3 that has been charged with the compensation voltage, maintains the compensation voltage of the third node N3 uniform even when the 12th and 13th transistors M12 and M13 are turned off in the second period.

The second buffer **260j** supplies the compensation voltage applied to the third node N3 to the voltage generator **240j** at the fourth node N4. The voltage generator **240j** divides the voltage difference between the voltage of the reference power source V_{ref} and the compensation voltage into a number of different gray scale voltages V(0) to V(2^k-1). The compensation voltage applied to the third node N3 may be the same or may vary in each pixel **1401** due to the mobility of the transistors included in the pixel **1401**. The compensation voltages supplied to the j voltage generators **2401** to **240j** at each point time are determined by the pixels **1401** to which the data lines D1 to Dj are coupled at that point in time.

On the other hand, if different compensation voltages are supplied to the voltage generators **2401** to **240j**, the values of the gray scale voltages V(0) to V(2^k-1) supplied to the DACs **2501** to **250j** provided in the j channels are also different from one another. Since the gray scale voltages V(0) to V(2^k-1) are controlled by the pixels to which the data lines D1 to Dj are currently coupled, although the mobility of the transistors included in the pixels **1401** or **1402** is non-uniform, the display region **130** can display images with a substantially uniform brightness.

FIG. 14 illustrates driving waveforms supplied to the switching unit, the current sink unit, the precharging unit, and the pixel illustrated in FIG. 13.

The voltage value of the data signal DS supplied to the pixel **140** will be described in detail with reference to FIGS. 13 and 14. First, the scan signal is supplied to the (n-1)th scan line Sn-1. When the scan signal is supplied to the (n-1)th scan line Sn-1, the third and fifth transistors M3 and M5 are turned on. Then, the voltage value obtained by subtracting the threshold voltage of the fourth transistor M4 from the first power source ELVDD is applied to the second node N2 and the voltage of the reference power source V_{ref} is applied to the first node N1. At this time, the voltage corresponding to

the voltage drop of the first power source ELVDD and the threshold voltage of the fourth transistor M4 are charged in the second capacitor C2.

The voltages applied to the first node N1 and the second node N2 may be represented by EQUATION 1. However, in a period between the point of time where the scan signal supplied to the (n-1)th scan line Sn-1 is turned off and the point of time where the scan signal is supplied to the nth scan line Sn, the first and second nodes N1 and N2 float. Therefore, the value of the voltage charged in the second capacitor C2 does not change.

Then, the scan signal is supplied to the nth scan line Sn so that the first and second transistors M1 and M2 are turned on. In the portion of the 0th period when the scan signal is supplied to the nth scan line Sn, the 15th and 11th transistors M15 and M11 are also turned on by their respective control signals CS4 and CS1. When the 15th and 11th transistors M15 and M11 are turned on, the precharging voltage Vp is supplied to the first node N1 via the 15th transistor M15, the first buffer 270j, the 11th transistor M11, the data line Dj, and the first transistor M1. As a result, the voltage corresponding to the precharging voltage Vp is charged in the first capacitor C1.

Here, the value of the precharging voltage Vp is determined to correspond to the value of the current source Imax. The value of the precharging voltage Vp is set so that a current corresponding to the current source Imax can flow through the fourth transistor M4. That is, the value of the precharging voltage Vp is set so that the current obtained when the pixel 1401 emits light with the maximum brightness flows through the fourth transistor M4.

Then, the 12th and 13th transistors M12 and M13 are turned on in the first period of the horizontal period H by their common control signal CS2. When the 12th and 13th transistors M12 and M13 are turned on, the current that flows through the current source Imax via the first power source ELVDD, the fourth transistor M4, the second transistor M2, the data line Dj, and the 13th transistor M13 sinks into this current source.

At this time, the current of the current source Imax through the fourth transistor M4, is obtained by EQUATION 2. The voltage applied to the second node N2 when the current obtained by EQUATION 2 flows through the fourth transistor M4 may be represented by EQUATION 3.

The voltage applied to the first node N1 by the coupling of the second capacitor C2 may be represented by EQUATION 4.

The voltage V_{N1} applied to the first node N1 is ideally the same as the voltage V_{N3} applied to the third node N3 and the voltage V_{N4} applied to the fourth node N4. That is, when the current is sunk by the current source Imax, the voltage obtained by EQUATION 4 is applied to the fourth node N4. On the other hand, since a predetermined voltage is charged in the first capacitor C1 by the precharging voltage Vp in the 0th period, it is possible to minimize the length of time for which the voltage obtained by EQUATION 4 is applied to the fourth node N4.

As illustrated in EQUATION 4, the voltage applied to the third and fourth nodes N3 and N4 is affected by the electron mobility of the transistors included in the pixel 140 the current from which sinks. Therefore, the voltage value applied to the third and fourth nodes N3 and N4 when the current is sunk by the current source Imax varies in each of the pixels 140 (or 1401 or 1402).

On the other hand, when the voltage obtained by EQUATION 4 is applied to the fourth node N4, the voltage V_{diff} across the voltage generator 240j may be represented by EQUATION 5.

When the DAC 250j selects the hth (h is a natural number no more than f) gray scale voltage among f (f is a natural number) gray scale voltages in response to the data Data, the voltage Vb supplied to the first buffer 270j may be represented by EQUATION 6.

However, after the current sinks in the first period so that the voltage obtained by EQUATION 4 is charged in the third capacitor C3, the 12th and 13th transistors M12 and M13 are turned off and the 14th and 11th transistors M14 and M11 are turned on in the second period. At this time, the third capacitor C3 maintains the voltage charged in the capacitor. Therefore, the voltage value of the third node N3 may be maintained as illustrated in EQUATION 4.

Since the 14th and 11th transistors M14 and M11 are turned on in the second period of the horizontal period H, the data signal selected by the DAC 250j is supplied to the first node N1 via the first buffer 270j, the data line Dj, and the first transistor M1. That is, the voltage obtained by EQUATION 6 is supplied to the first node N1. The voltage applied to the second node N2 by the coupling of the second capacitor C2 may be represented by EQUATION 7.

At this time, the current that flows via the fourth transistor M4 may be represented by EQUATION 8.

Referring to EQUATION 8, according to the present invention, the current that flows through the fourth transistor M4 is determined by the gray scale voltage generated by the voltage generator 240j. That is, according to the present invention, the current determined by the gray scale voltage can flow to the fourth transistor M4 regardless of the threshold voltage and electron mobility of the fourth transistor M4. Therefore, it is possible to display images with a substantially uniform brightness. Also, according to the present invention, since the precharging voltage Vp is supplied to the pixel 140 (or pixel 1401 or pixel 1402) in the 0th period, it is possible to reduce the driving time of the first period in which the current sinks.

As described above, according to the data driver of the embodiments of the present invention, the organic light emitting display device using the data driver, and the method of driving the organic light emitting display device, since the values of the gray scale voltages generated by the voltage generator are reset using the compensation voltage generated when the current from the pixel sinks and the reset gray scale voltages are supplied to the pixel the current from which sinks, it is possible to display images with a substantially uniform brightness regardless of the electron mobility of the transistors. According to the present invention, since the precharging voltage is supplied before the currents sink, it is possible to reduce the time for which the currents sink and to stably drive the organic light emitting display device.

Although certain exemplary embodiments of the present invention have been shown and described, it would be appreciated by those skilled in the art that changes might be made to these embodiments without departing from the principles and spirit of the invention, the scope of which is defined in the claims and their equivalents.

What is claimed is:

1. A data driver for an organic light emitting display device comprising:

- a plurality of current sink units configured to receive predetermined currents flowing through data lines and through transistors respectively, the transistors being included in pixels;
- a plurality of voltage generators for resetting gray scale voltages using compensation voltages corresponding to the predetermined currents and electron mobility of the transistors, the compensation voltages being for compensating for the electron mobility of the transistors;

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a plurality of digital-to-analog converters for selecting one gray scale voltage among the gray scale voltages as a data signal in response to a bit value of data supplied from outside of the data driver to the data driver; and a plurality of switching units for supplying the data signal to the data lines, wherein each of the compensation voltages subtracted by a reference voltage is proportional to a square root of the corresponding predetermined current divided by the corresponding electron mobility.

2. The data driver as claimed in claim 1, wherein the current sink units receive the predetermined currents from pixels coupled to the data lines.

3. The data driver as claimed in claim 2, wherein the current sink units receive the predetermined currents in a first period, the first period being a part of a horizontal period.

4. The data driver as claimed in claim 3, wherein each of the current sink units comprises:

- a current source for receiving one of the predetermined currents;
- a first transistor located between one of the data lines and the voltage generator, the first transistor being turned on in the first period;
- a second transistor located between said one of the data lines and the current source, the second transistor being turned on in the first period; and
- a capacitor coupled to the second transistor and charged with one of the compensation voltages applied to the first transistor when said one of the predetermined currents flows to said one of the data lines,

wherein a gate electrode of the first transistor is directly coupled to a gate electrode of the second transistor.

5. The data driver as claimed in claim 3, wherein the switching units couple the data lines and the digital-to-analog converters to each other in a second period of the horizontal period occurring after the first period.

6. The data driver as claimed in claim 5, wherein each of the switching units comprises at least one transistor turned on in the second period.

7. The data driver as claimed in claim 6, wherein each of the switching units comprises two transistors, and wherein the two transistors are coupled to each other in a form of a transmission gate.

8. The data driver as claimed in claim 3, further comprising at least one precharging unit for supplying a precharging voltage to a pixel coupled to the data line in a 0th period before the first period.

9. The data driver as claimed in claim 2, wherein values of the predetermined currents are equal to values of currents that flow when the pixels emit light with a maximum brightness.

10. The data driver as claimed in claim 1, wherein each of the voltage generators comprises a plurality of voltage divid-

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ing resistors coupled between a first terminal and a second terminal for generating the gray scale voltages.

11. The data driver as claimed in claim 10, wherein the first terminal receives a reference voltage from a reference power source, and wherein the second terminal receives one of the compensation voltages.

12. The data driver as claimed in claim 1, further comprising:

- first buffers located between the digital-to-analog converters and the switching units; and
- second buffers located between the current sink units and the voltage generators.

13. The data driver as claimed in claim 1, further comprising:

- a shift register unit including shift registers for generating sampling signals;
- a sampling latch unit including a plurality of sampling latches for receiving the data supplied to the data driver in response to the sampling signals; and
- a holding latch unit including holding latches for receiving and storing the data stored in the sampling latches and for supplying the data stored in the holding latches to the digital-to-analog converters.

14. The data driver as claimed in claim 13, further comprising a level shifter unit for increasing a voltage level of the data stored in the holding latches to supply the data to the digital-to-analog converters.

15. A method of driving an organic light emitting display device, the method comprising:

- controlling predetermined currents to flow in data lines coupled to pixels, the predetermined currents flowing through transistors respectively included in the pixels and being received by a plurality of current sink units;
- generating compensation voltages corresponding to the predetermined currents and electron mobility of the transistors, the compensation voltages being for compensating for the electron mobility of the transistors;
- resetting values of gray scale voltages using the compensation voltages; and
- selecting one voltage among the gray scale voltages corresponding to bit values of data supplied to a data driver from outside of the data driver, the selected voltage for being supplied to the data lines,

wherein each of the compensation voltages subtracted by a reference voltage is proportional to a square root of the corresponding predetermined current divided by the corresponding electron mobility.

16. The method as claimed in claim 15, wherein, the predetermined currents are equal to currents that flow when the pixels emit light with a maximum brightness.

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| 专利名称(译) | 数据驱动器，使用其的有机发光显示装置，以及驱动有机发光显示装置的方法 | | |
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| [标]申请(专利权)人(译) | RYU DO HYUNG 众博YONG 金弘KWON KWON OH KYONG | | |
| 申请(专利权)人(译) | 刘某DO HYUNG CHUNG, BO YONG KIM, HONG KWON Kwon, 啊庆 | | |
| 当前申请(专利权)人(译) | 三星DISPLAY CO., LTD. IUCF-HYU (产学合作基金会汉阳大学 | | |
| [标]发明人 | RYU DO HYUNG CHUNG BO YONG KIM HONG KWON KWON OH KYONG | | |
| 发明人 | RYU, DO HYUNG CHUNG, BO YONG KIM, HONG KWON KWON, OH KYONG | | |
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摘要(译)

能够显示具有基本均匀亮度的图像的数据驱动器，使用该数据驱动器的有机发光显示装置，以及驱动该有机发光显示装置的方法。数据驱动器包括：多个电流吸收单元，用于控制流过数据线的预定电流；多个电压发生器，用于使用在预定电流流动时产生的补偿电压来重置灰度级电压的值，多个数字 - 模拟用于响应于从外部提供的数据的比特值选择灰度级电压中的一个灰度级电压作为数据信号的转换器，以及用于将数据信号提供给数据线的多个开关单元。可以将预定电流设置为等于对应于最大亮度的像素电流。

